



Pavement Evaluation 2019



September 17-20, 2019
Roanoke, Virginia

Investigation of Profile-Based Curl and Warp Analysis Using LTPP Profile Data

By

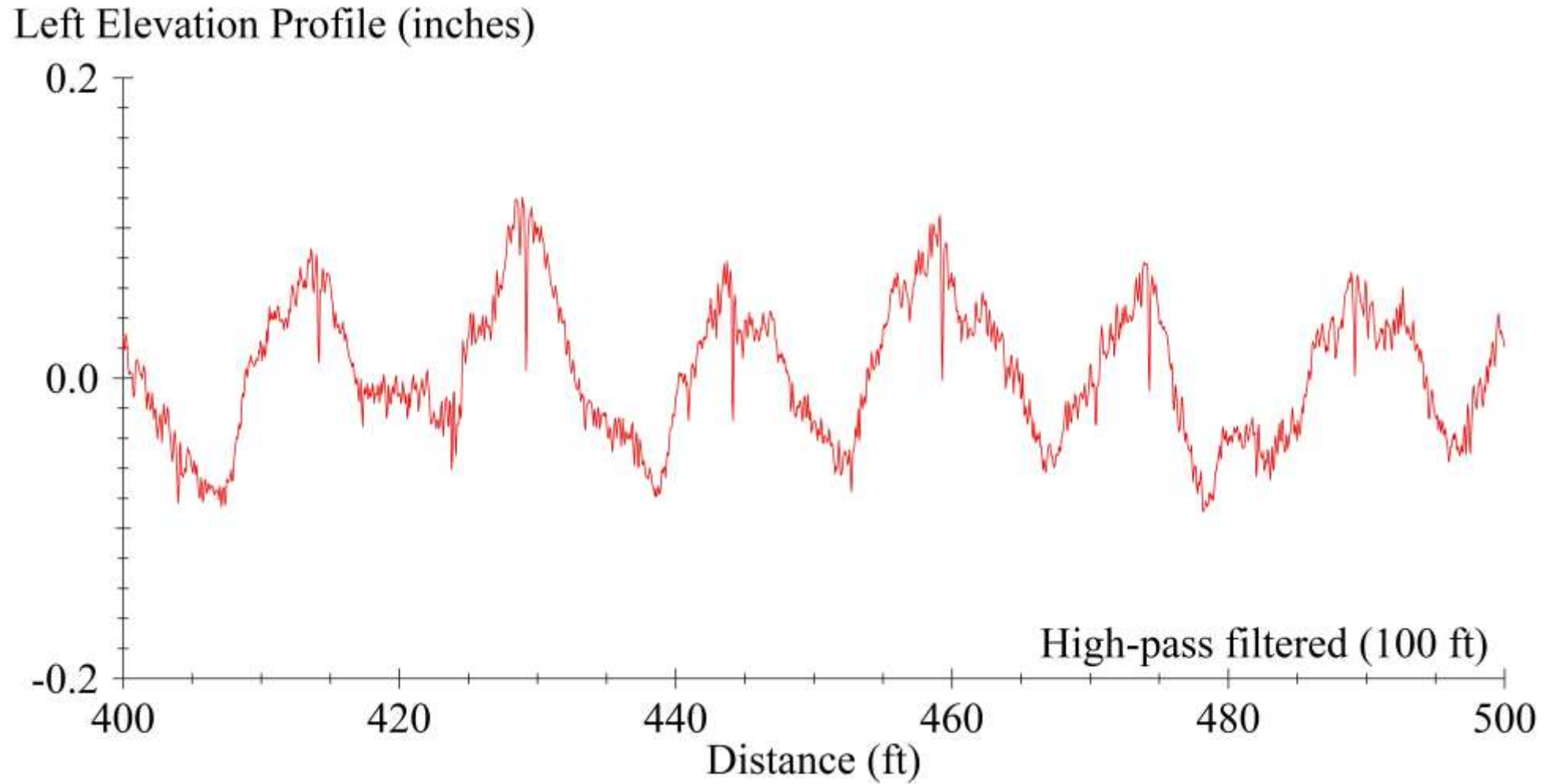
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University of Michigan Transportation Research Institute

With Kevin Senn and Timin Punnackal, NCE

And Larry Wisler, FHWA

AZ Section 040213, Upward Curl



Source: FHWA

PE 2019

Advancement of Curl and Warp.....

- Estimate the level of curl and warp of JPCPC using profile.
- Relate curl and warp to roughness.
- Refine an existing method.
- Apply the method to a broader set of sections.

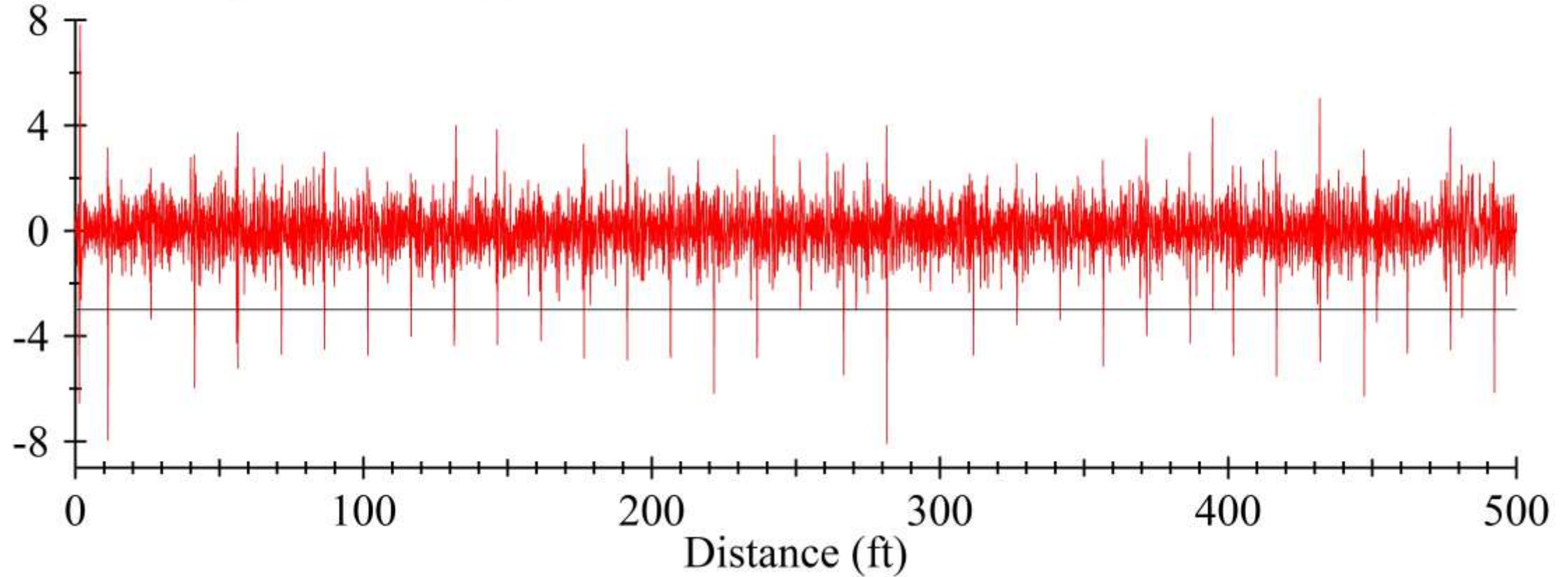
“What would the roughness be without curl and warp?”

Core Method (Chang, Rasmussen, et al.)

- Locate the joints.
- Isolate slab profiles.
- Fit slab profiles to an assumed function (Westergaard).
- Cast the result in terms of strain gradient.
- Aggregate over a test section.

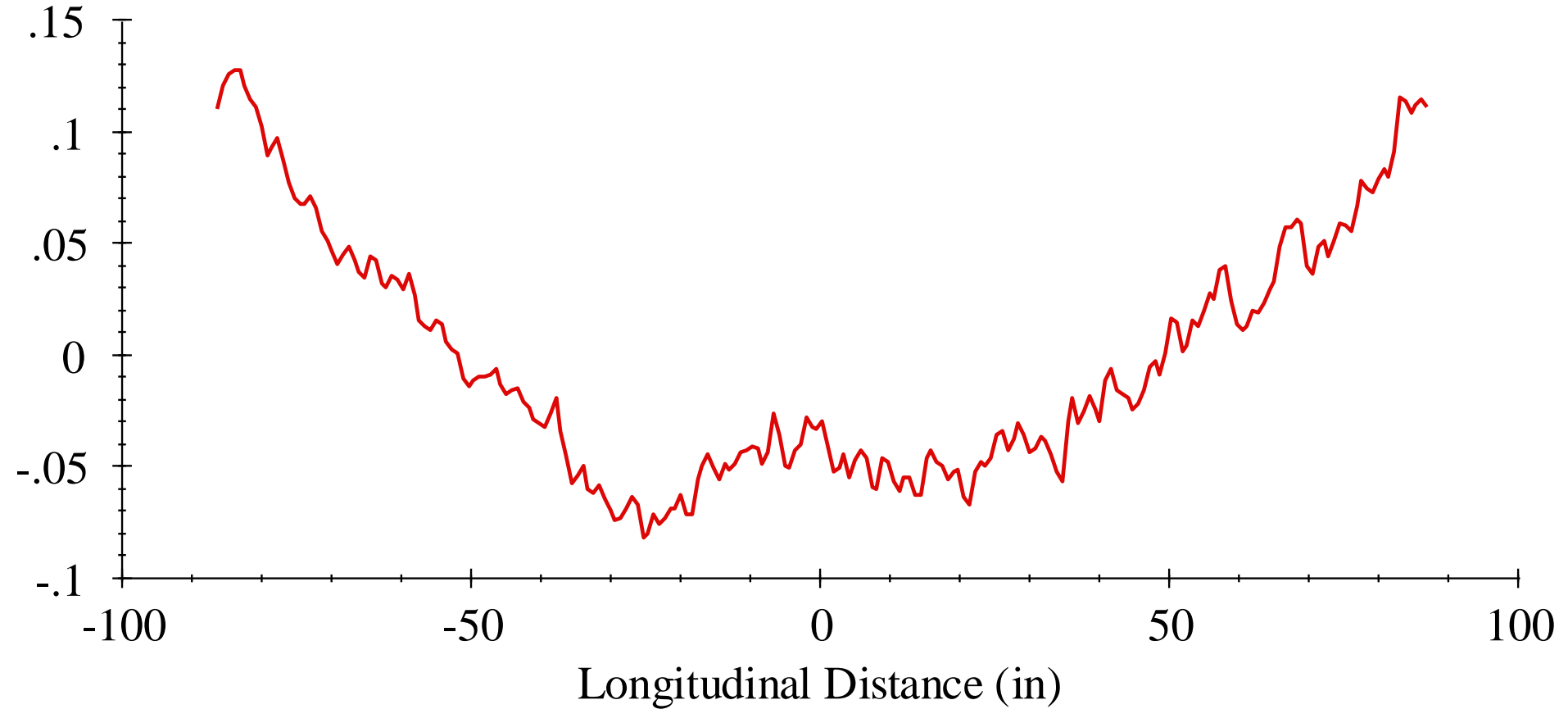
Joint Finding

Normalized Right Elevation (-)



Isolated Slab Profile

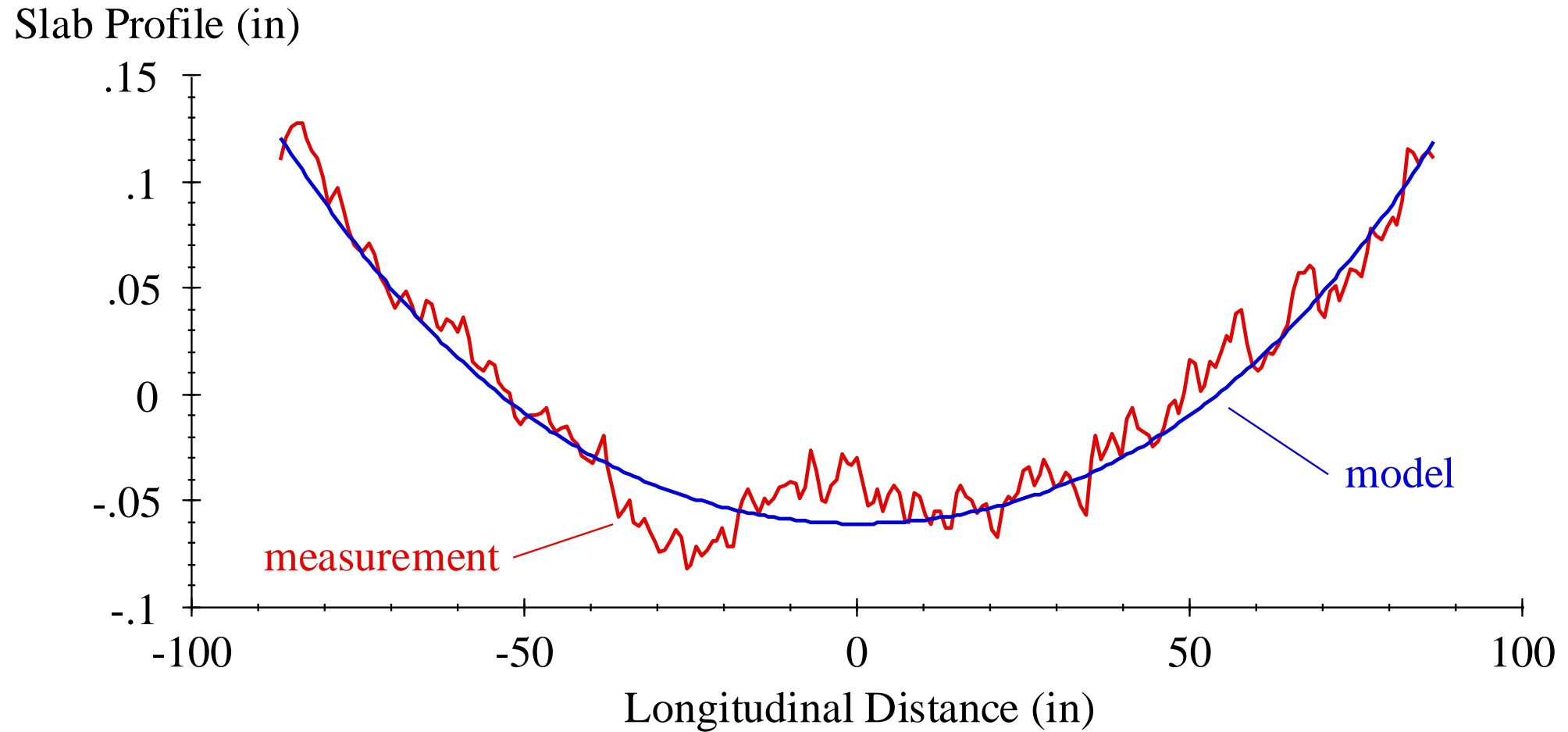
Detrended Profile (in)



Source: FHWA-HRT-12-068

PE 2019

Fitted Slab Profile



Source: FHWA-HRT-12-068

PE 2019

Westergaard Model

$$z = -z_0 \frac{2 \cos \lambda \cosh \lambda}{\sin 2\lambda - \sinh 2\lambda} \left[(-\tan \lambda + \tanh \lambda) \cos \frac{x}{l\sqrt{2}} \cosh \frac{x}{l\sqrt{2}} + (\tan \lambda + \tanh \lambda) \sin \frac{x}{l\sqrt{2}} \sinh \frac{x}{l\sqrt{2}} \right]$$

$$\lambda = \frac{b}{l\sqrt{8}}$$

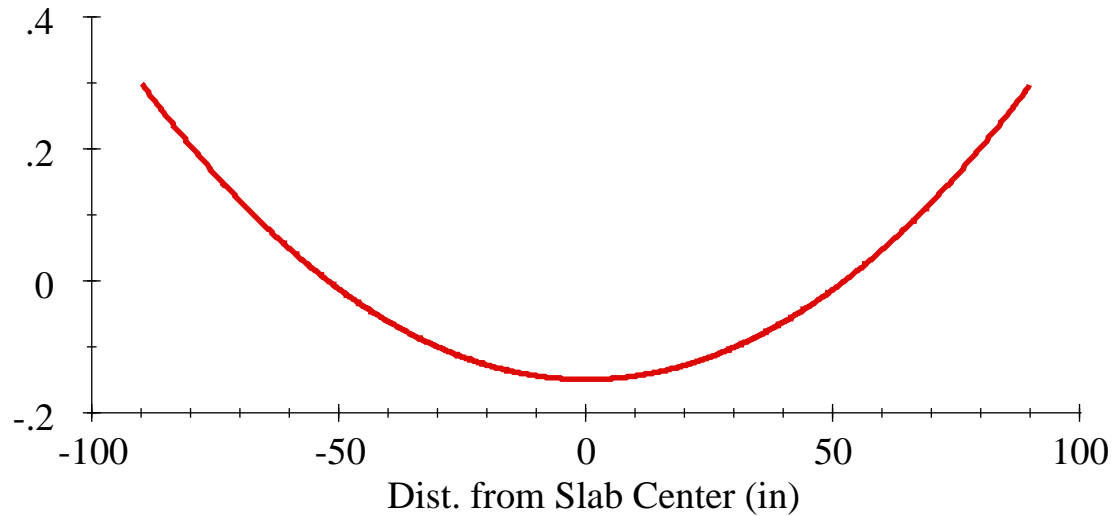
$$l = \sqrt[4]{\frac{Eh^3}{12(1-\mu^2)k}}$$

$$z_0 = \frac{-(1+\mu)(\alpha\Delta T + \Delta\varepsilon_{sh})}{h} l^2$$

$$PSG = \frac{(\alpha\Delta T + \Delta\varepsilon_{sh})}{h}$$

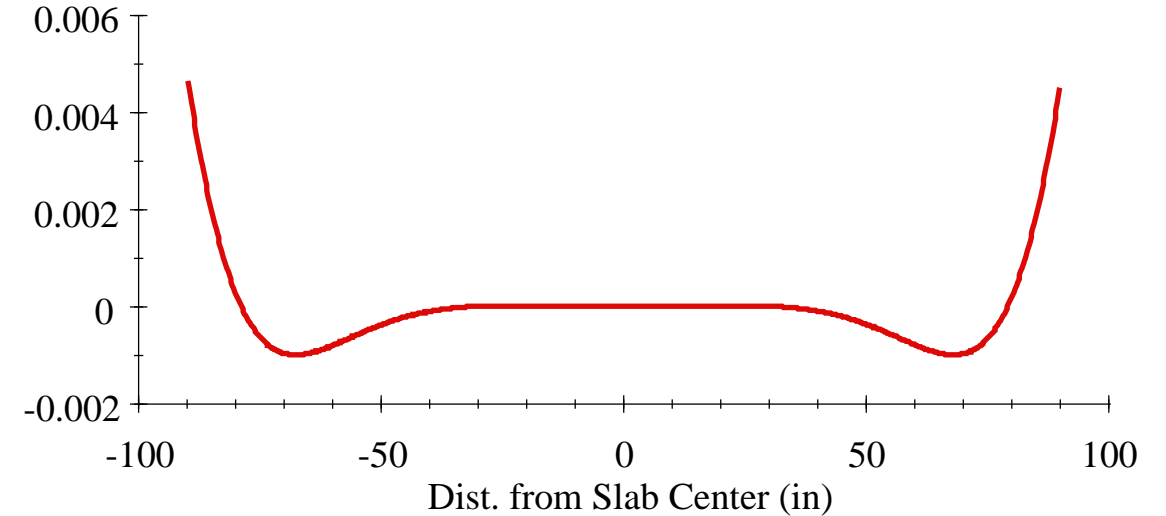
Idealized Slab Shapes

Vertical Slab Deformation (in)



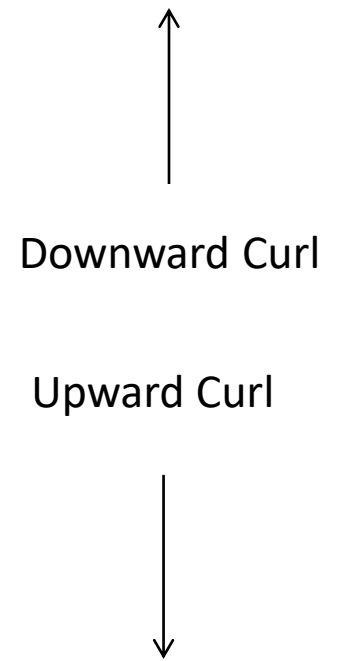
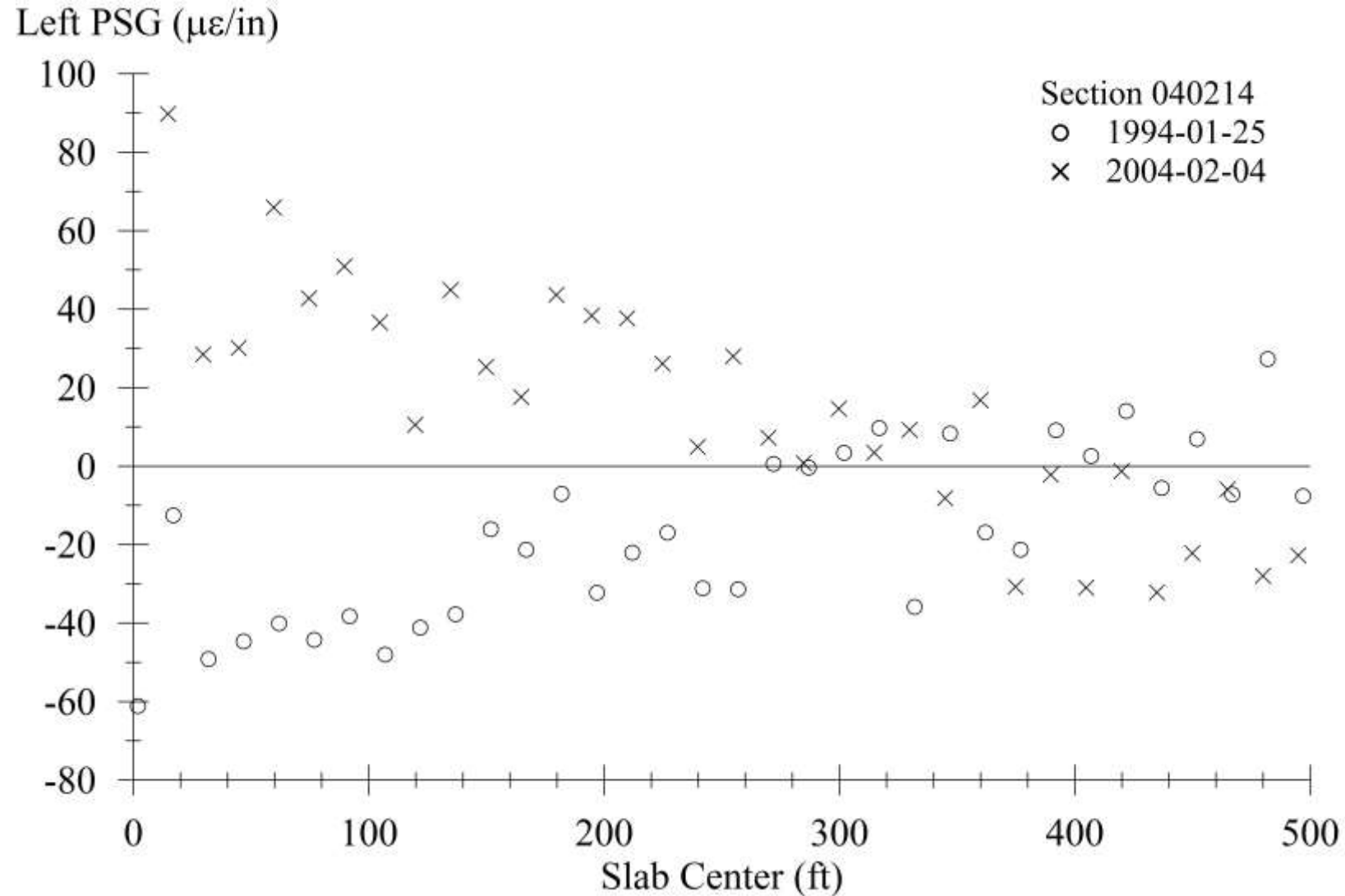
RRS (l) = 10 inches
PSG = $-40 \mu\epsilon/\text{inch}$

Vertical Slab Deformation (in)

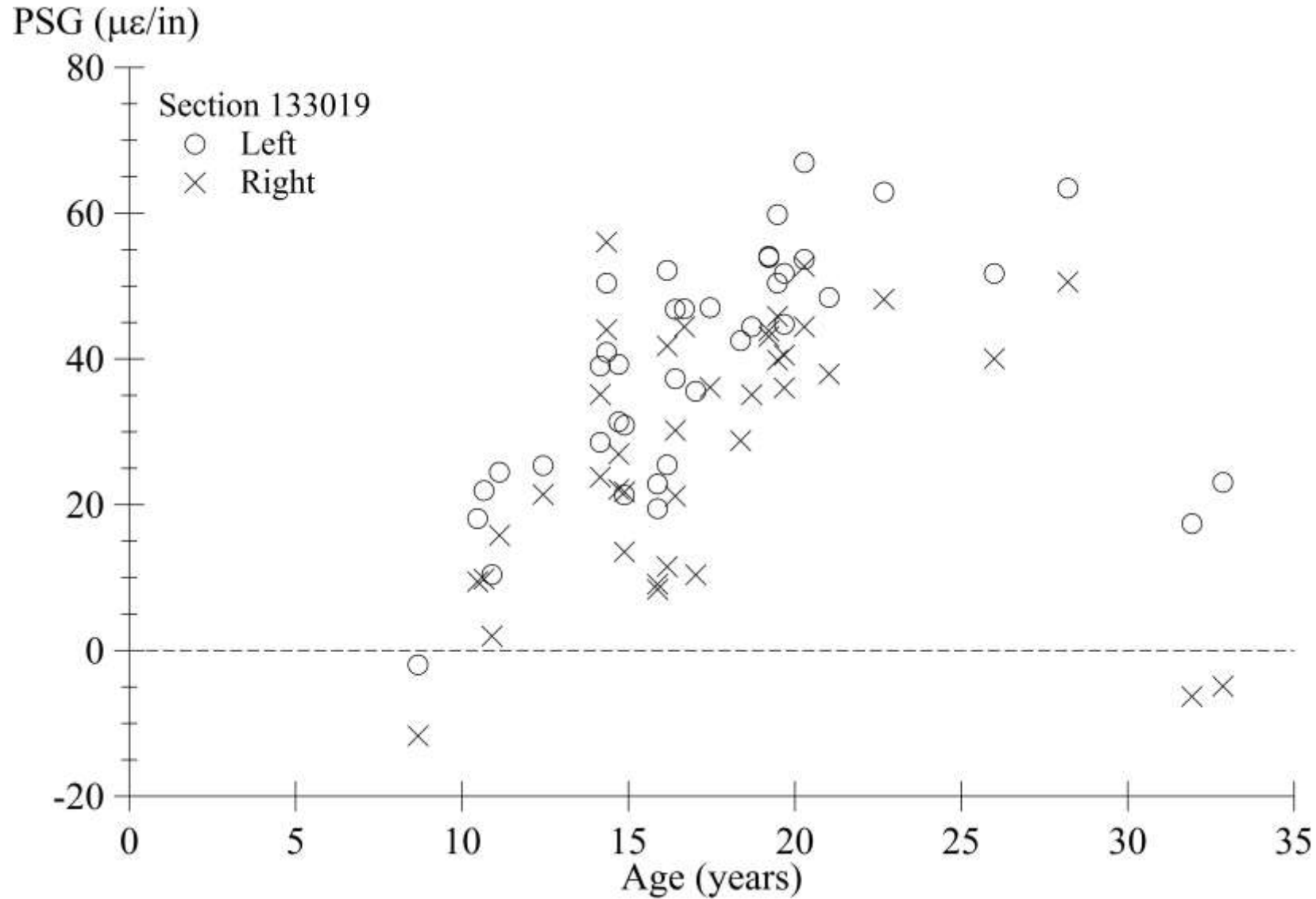


RRS (l) = 80 inches
PSG = $-40 \mu\epsilon/\text{inch}$

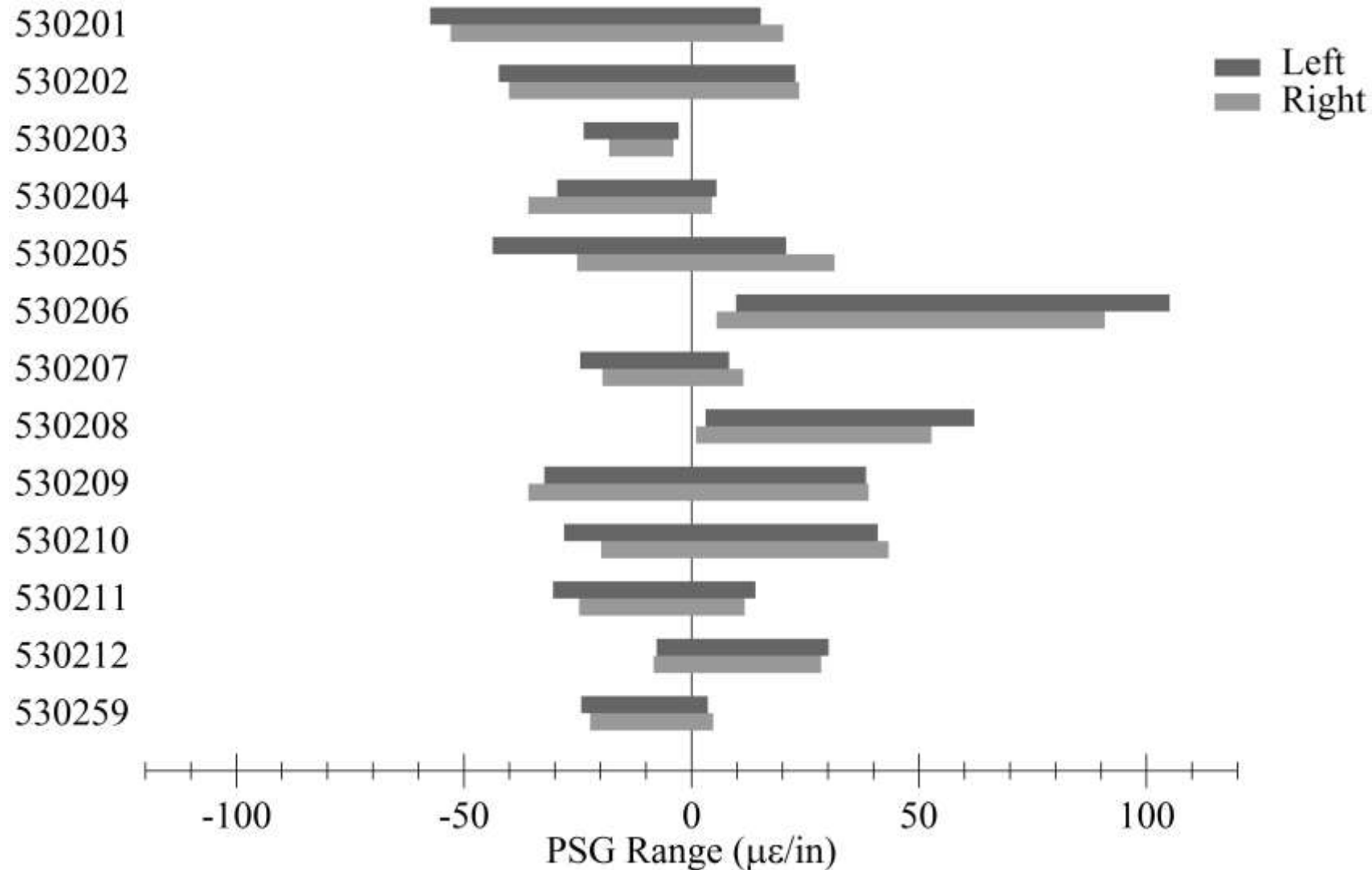
Structural Evaluation, Spatial Trends



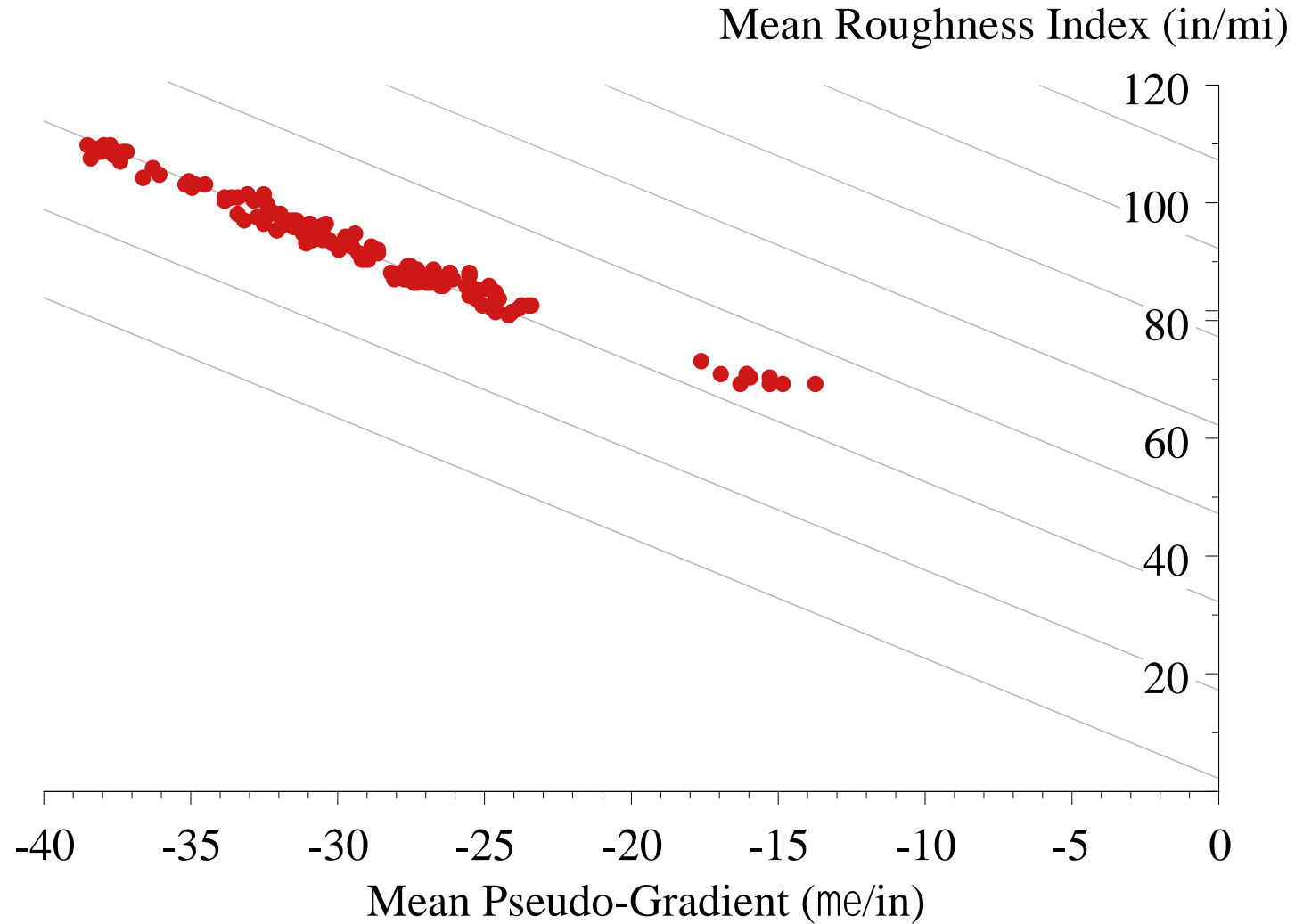
Structural Evaluation, Trends Over Time



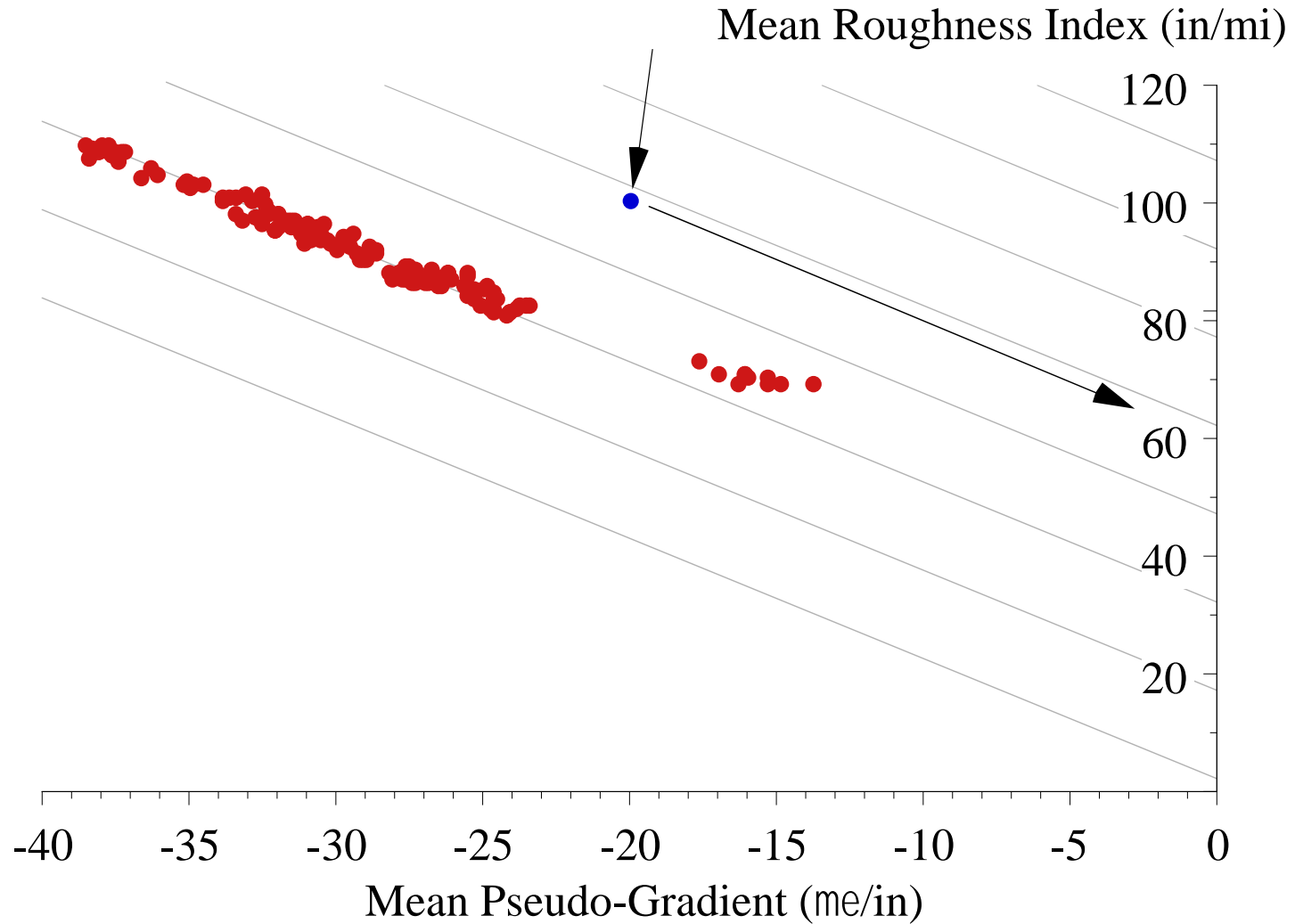
Structural Evaluation, by Test Section



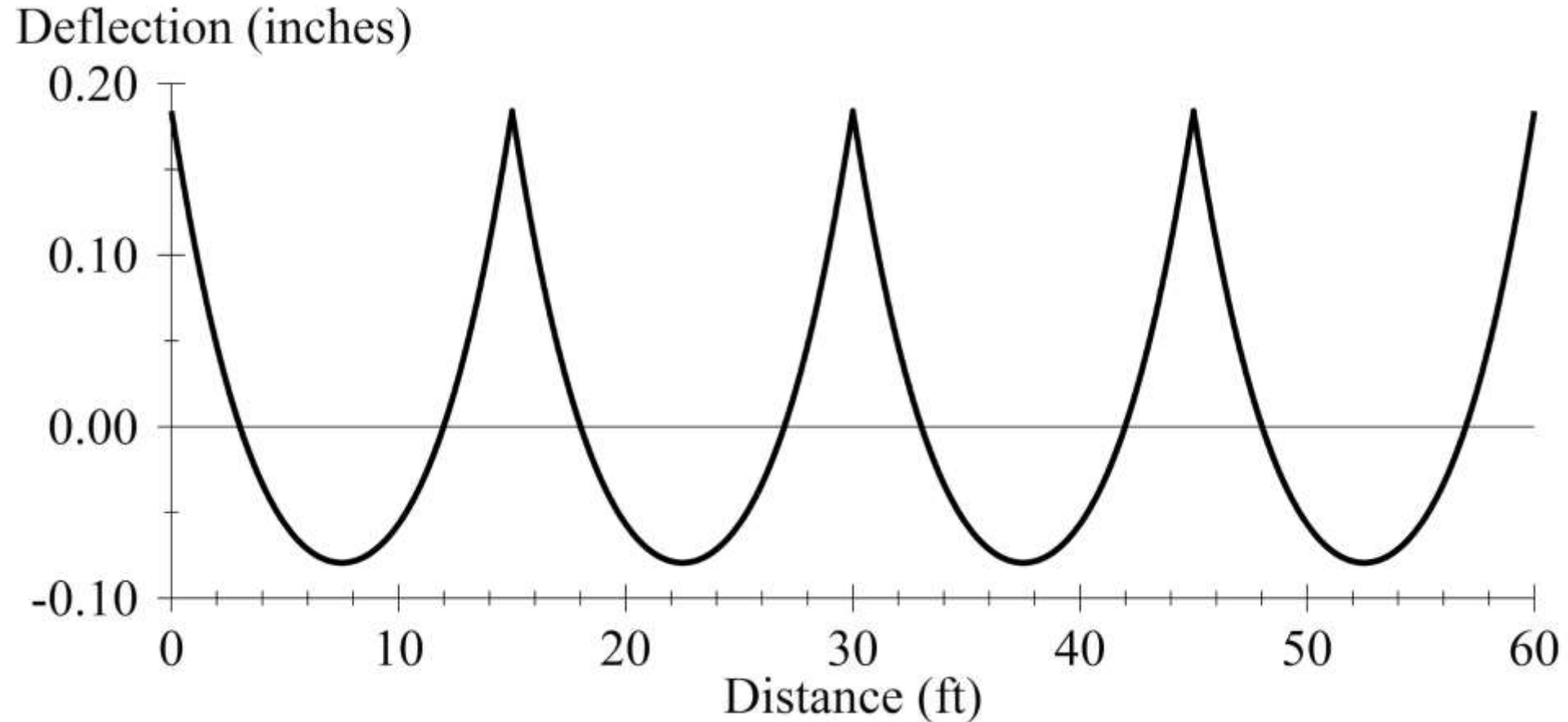
IRI Versus PSG, Hypothesis



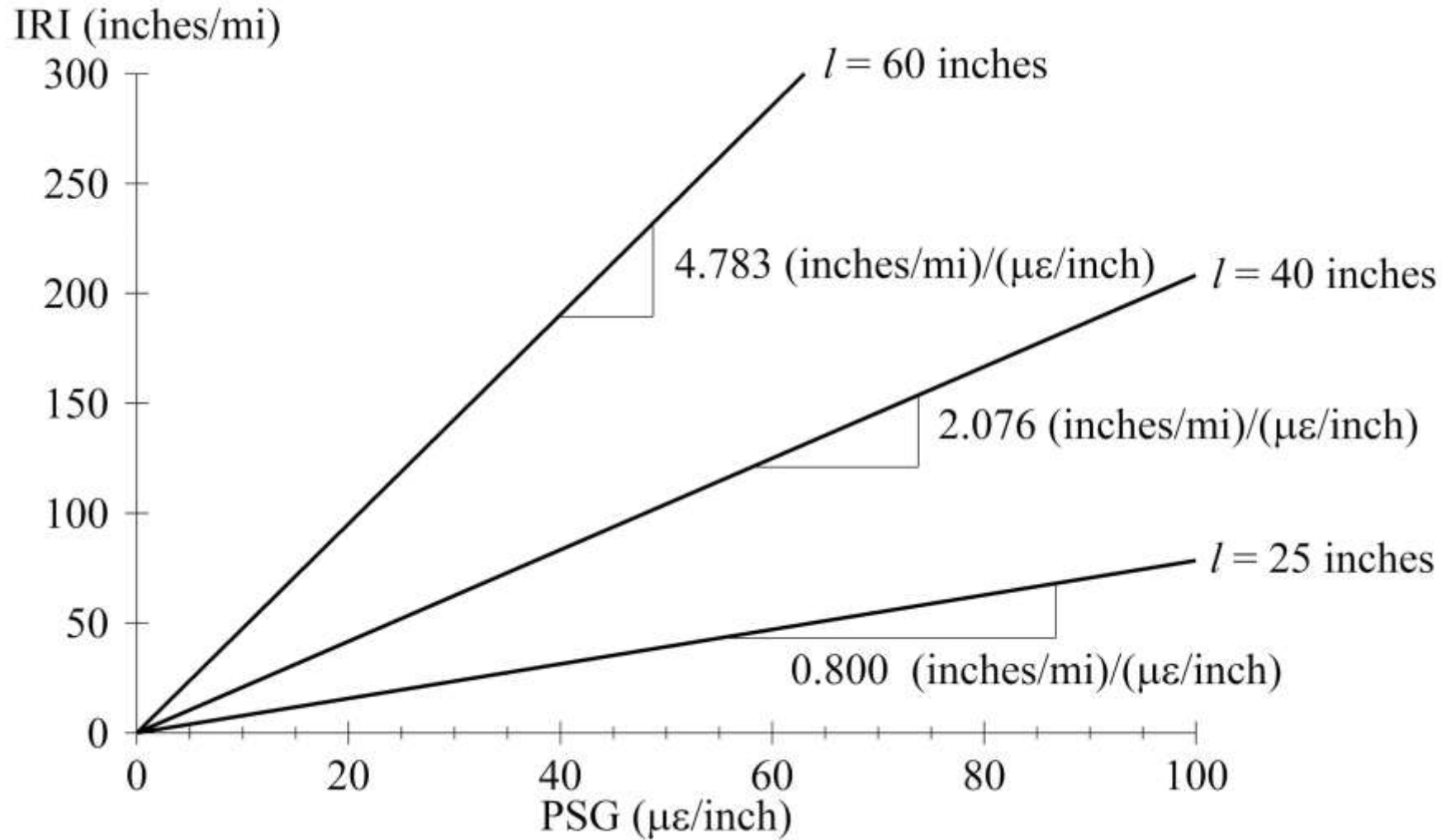
IRI Versus PSG, Hypothesis



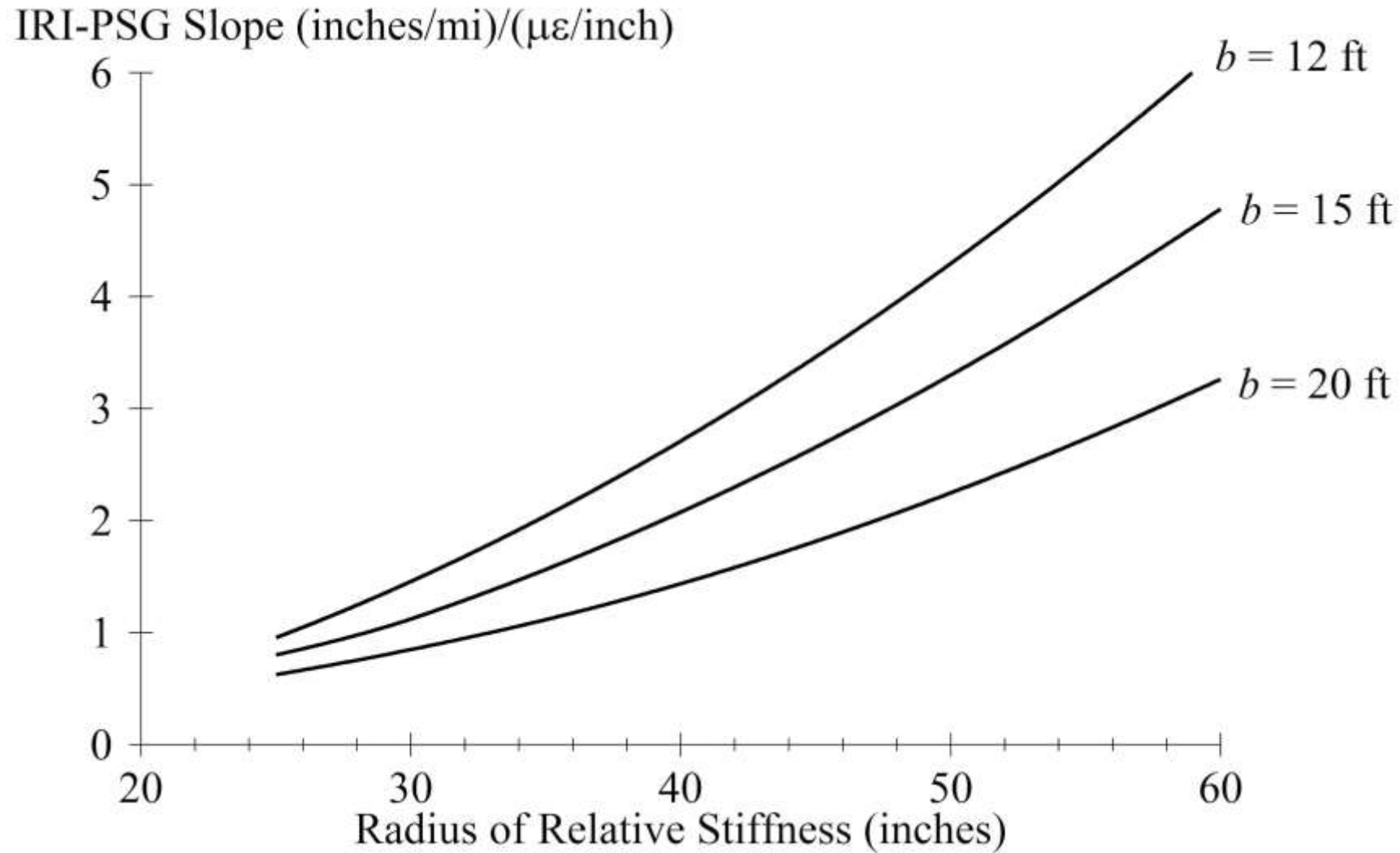
Idealized Profile ($l = 40$ inches)



IRI versus PSG



IRI/PSG Slope



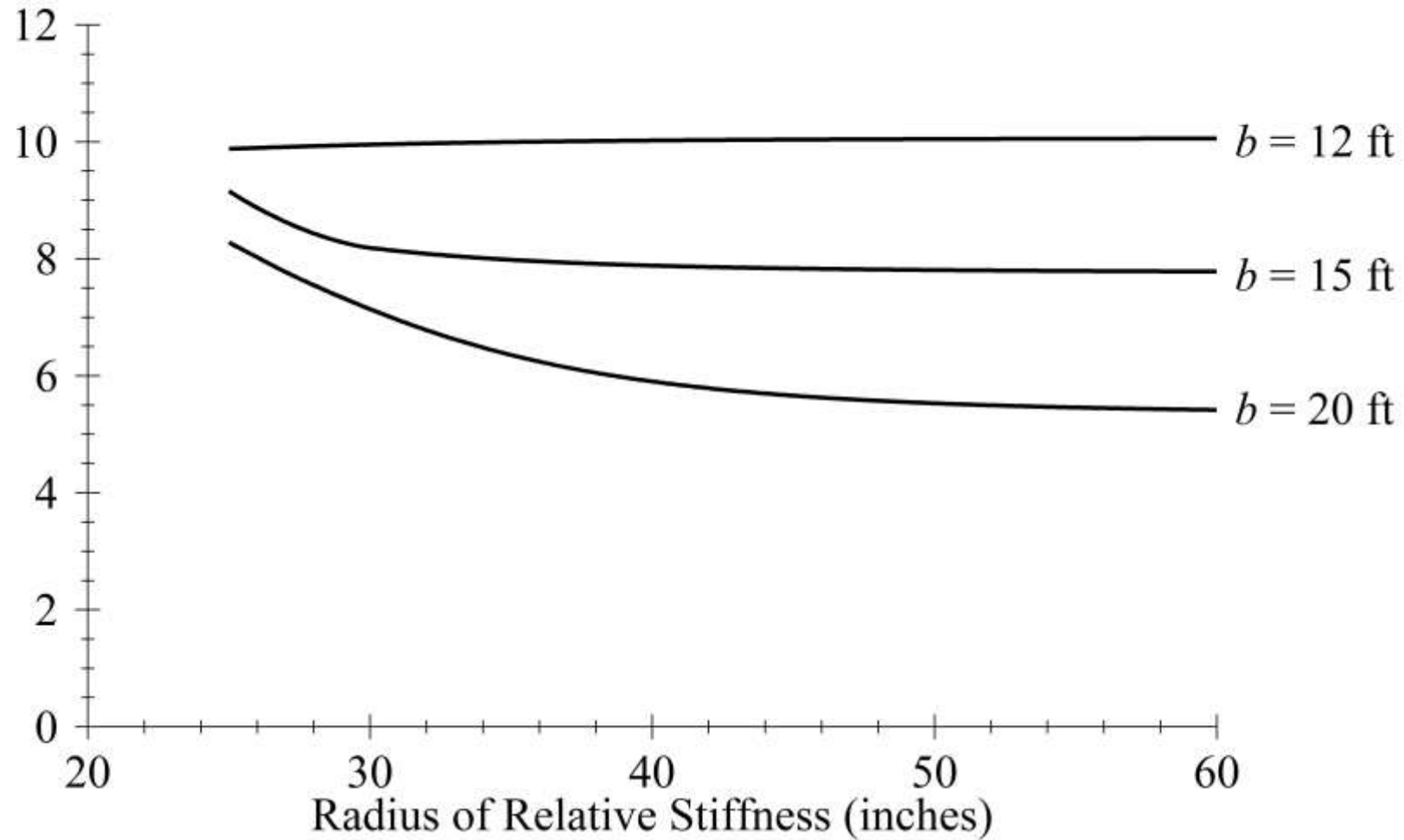
Uplift and PSG

$$z(x) = z_0 f(x, l, b) = -PSG(1 + \mu)l^2 f(x, l, b)$$

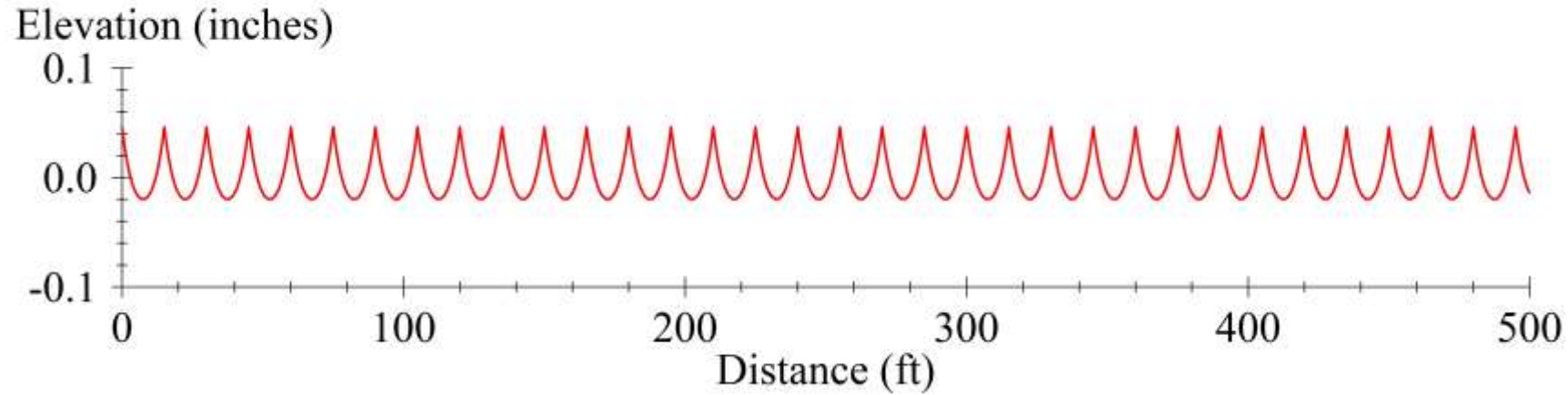
$$\Delta z = z(b / 2) - z(0) = -PSG(1 + \mu)l^2 \left(1 - \frac{s_\lambda c h_\lambda - c_\lambda s h_\lambda}{s_\lambda c_\lambda - s h_\lambda c h_\lambda} \right)$$

IRI Versus Uplift

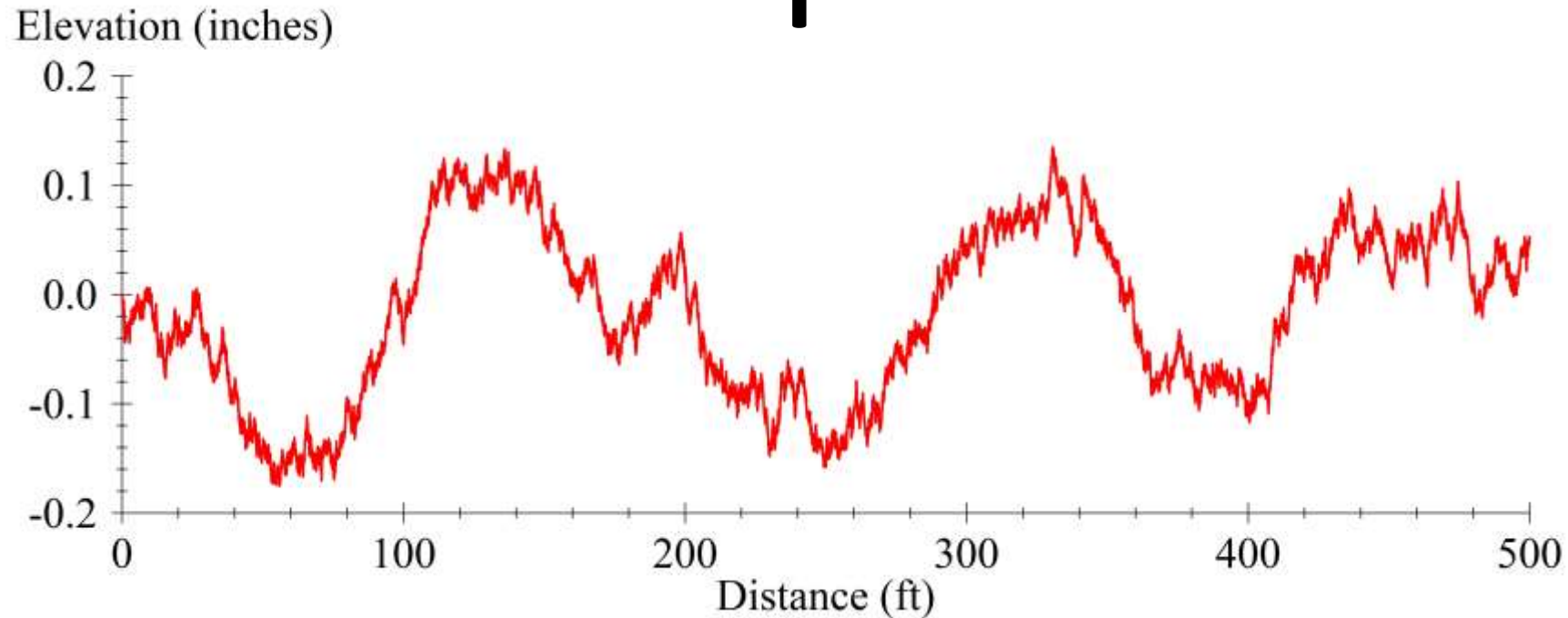
IRI per 0.01 inch of Relative Uplift (inches/mi)



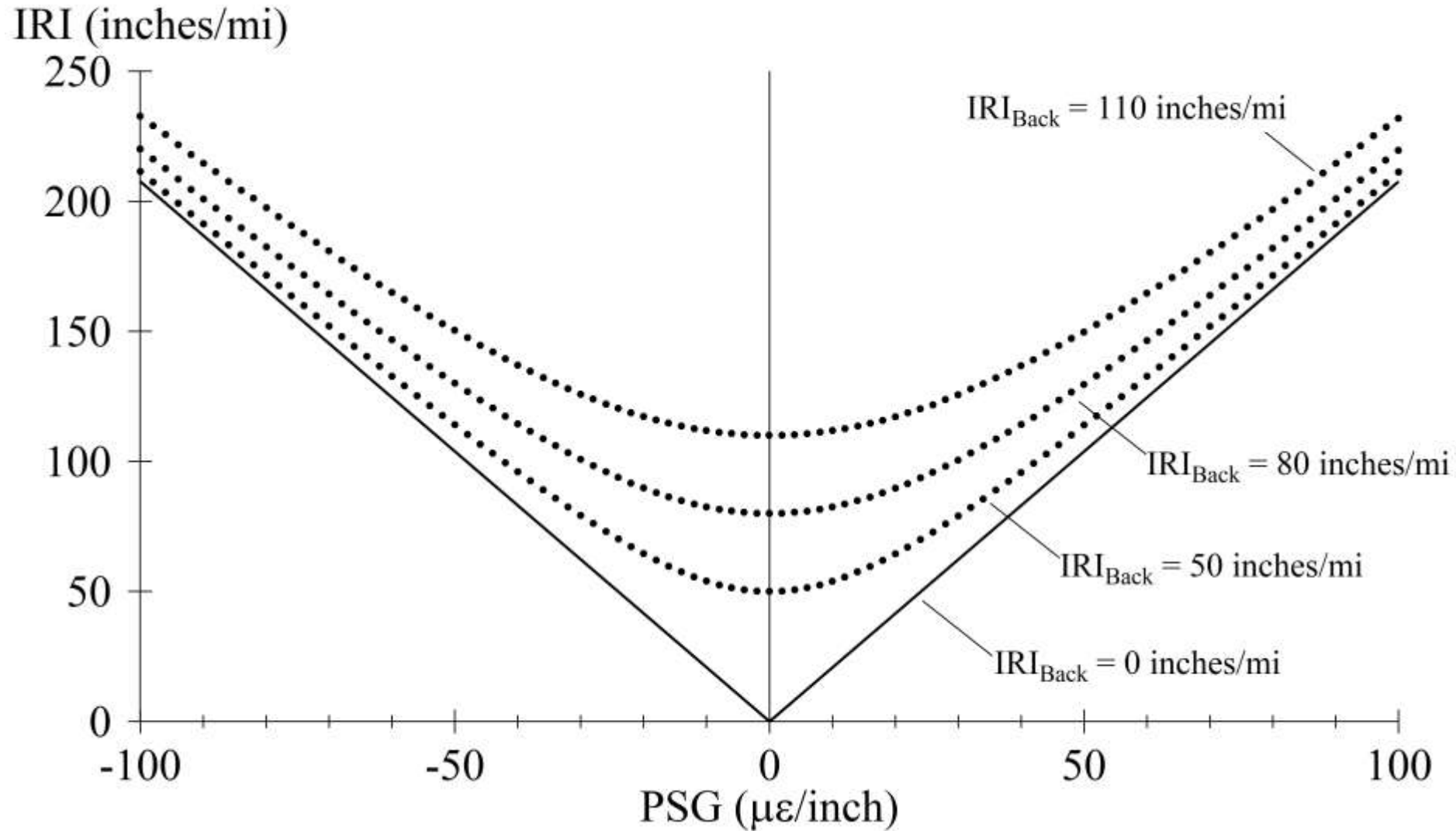
Idealized Curl and Background Roughness



+



Idealized Curl and Background Roughness



Idealized Curl and Background Roughness

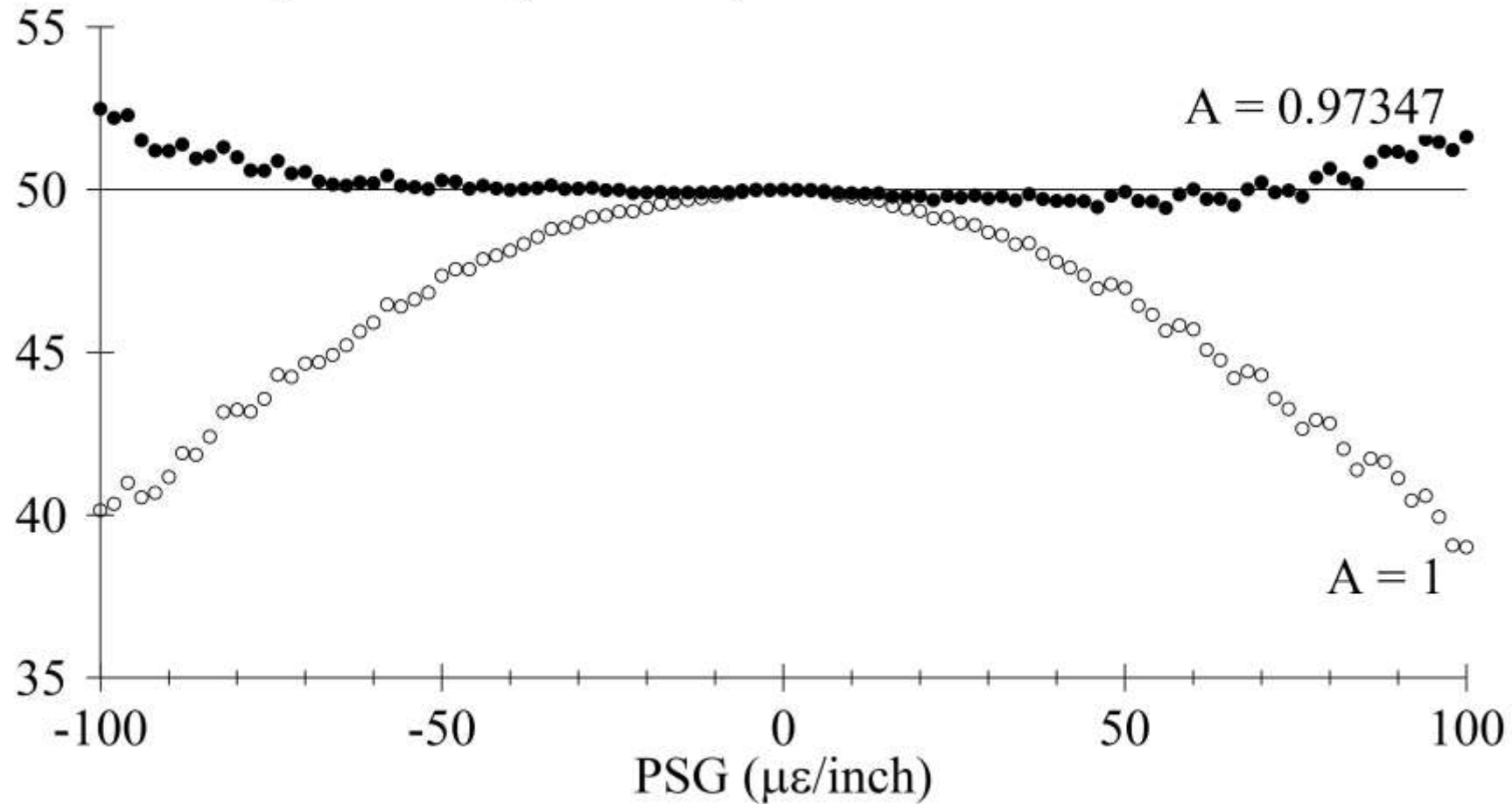
$$IRI_{Comb} = \sqrt{IRI_{Curl}^2 + IRI_{Back}^2}$$

$$IRI_{Comb} = \sqrt{\left(PSG \frac{dIRI}{dPSG}\right)^2 + IRI_{Back}^2}$$

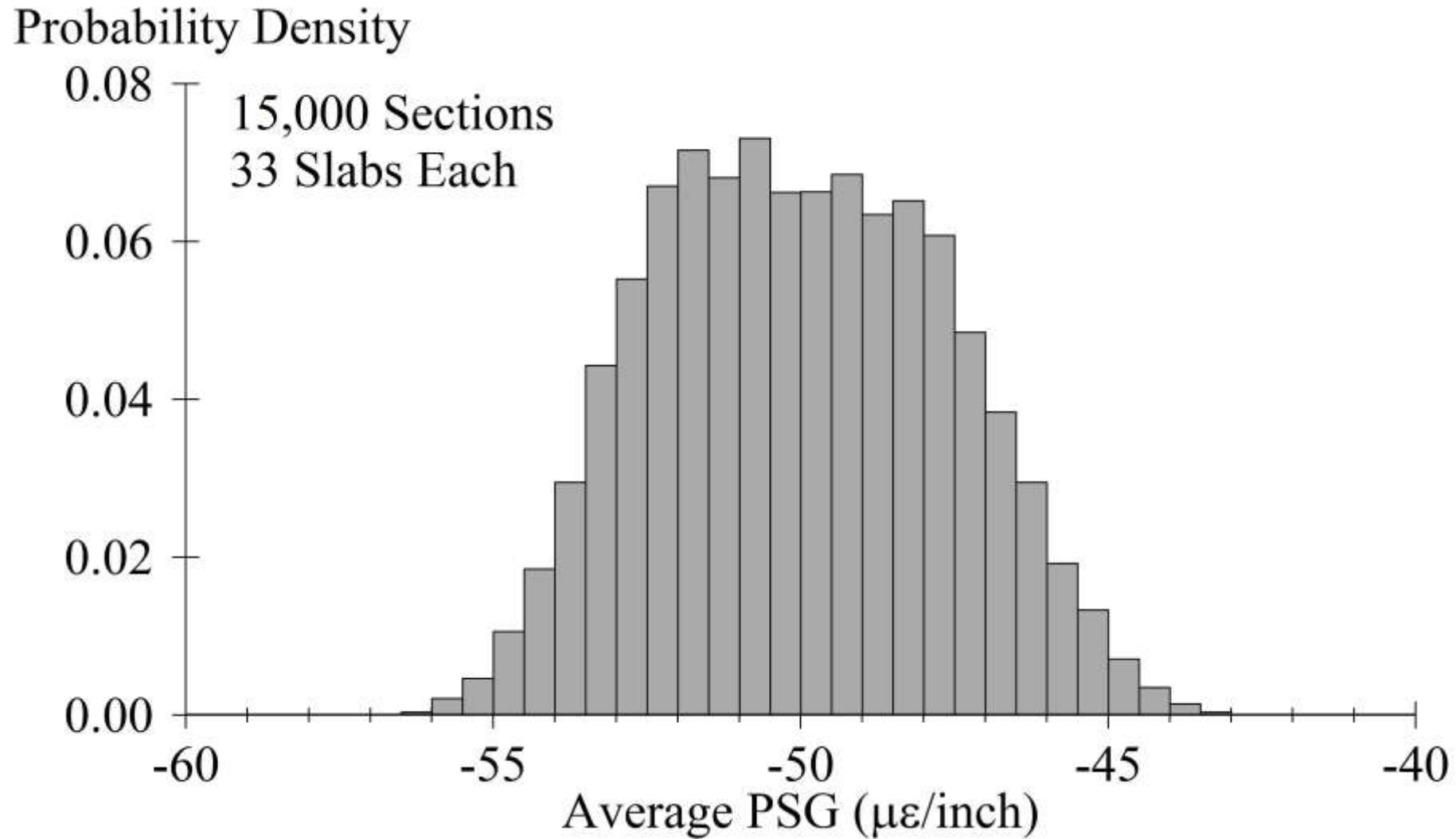
Background Roughness

$$IRI_{Back} = \sqrt{IRI_{Comb}^2 - A \left(PSG \frac{dIRI}{dPSG} \right)^2}$$

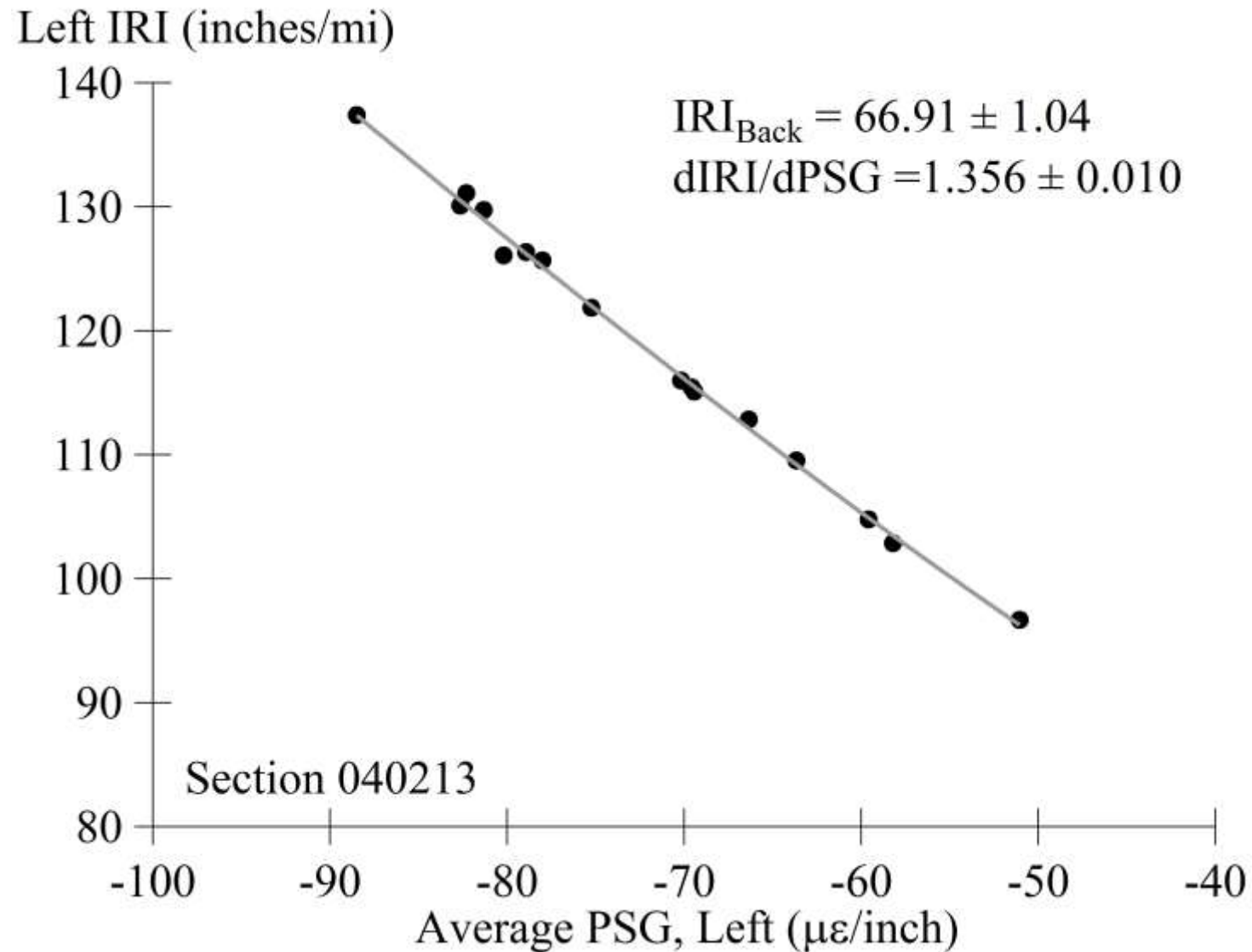
Predicted Background IRI (inches/mi)



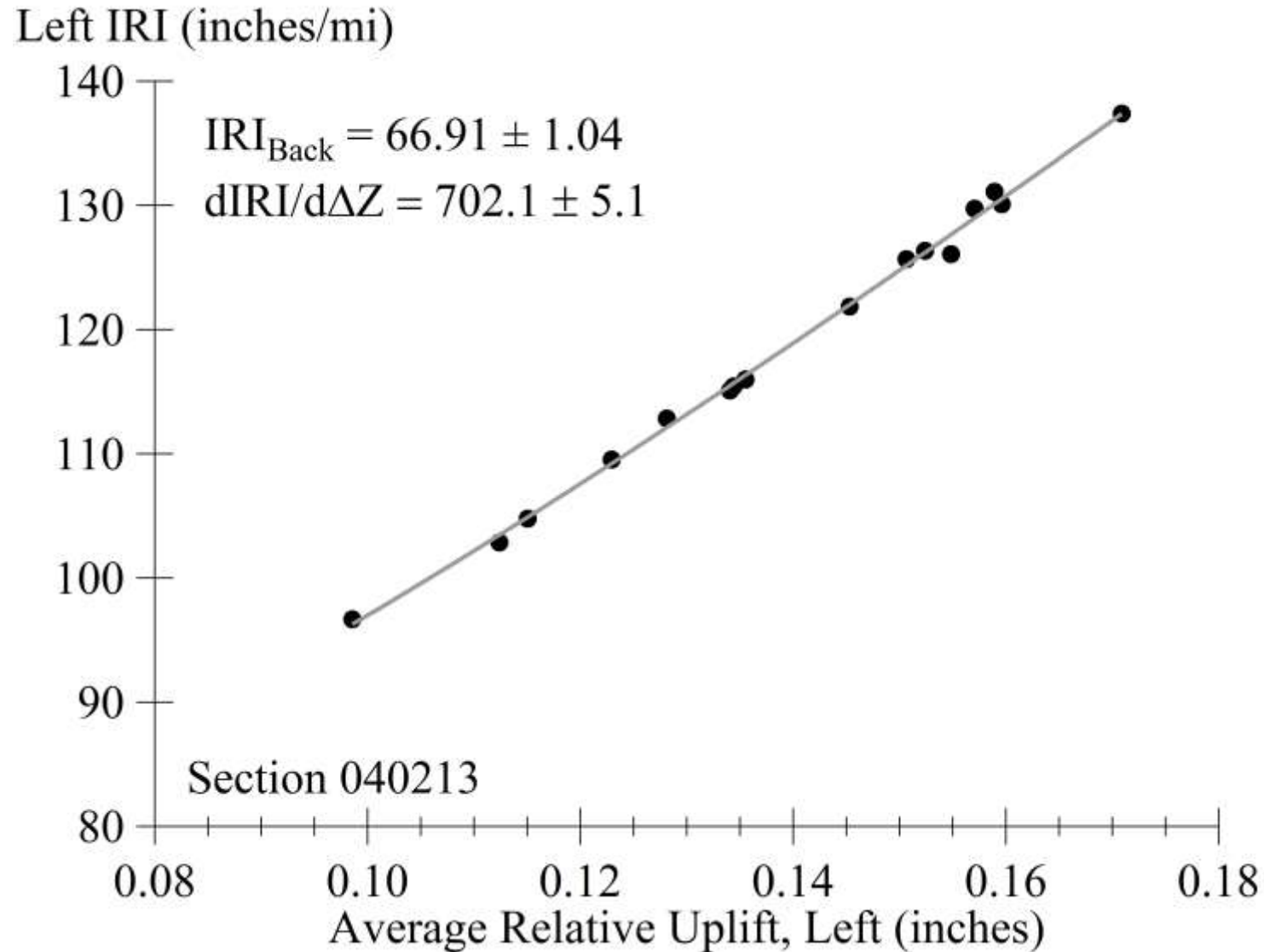
Section-Wide PSG Average



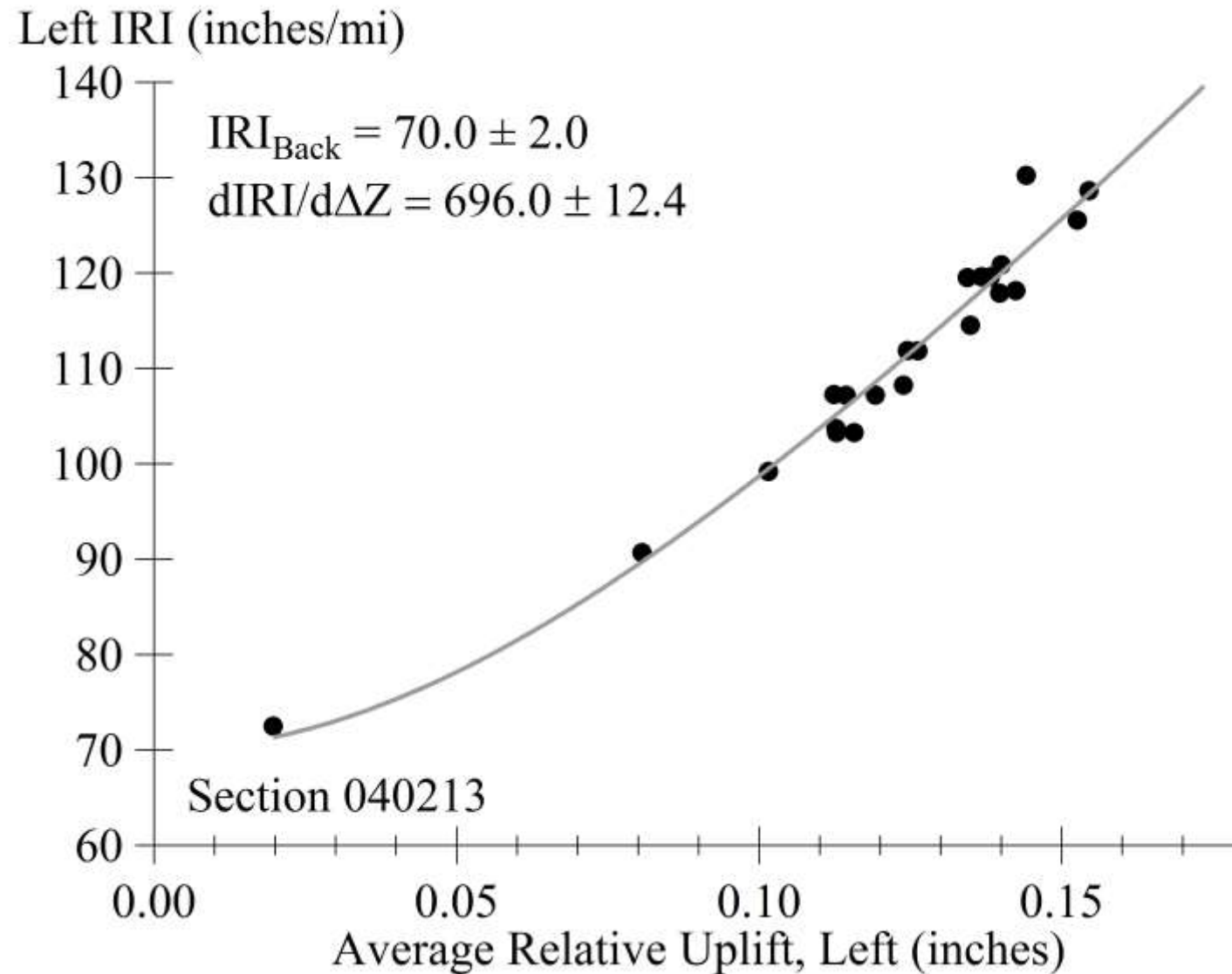
IRI versus PSG, FHWA Data



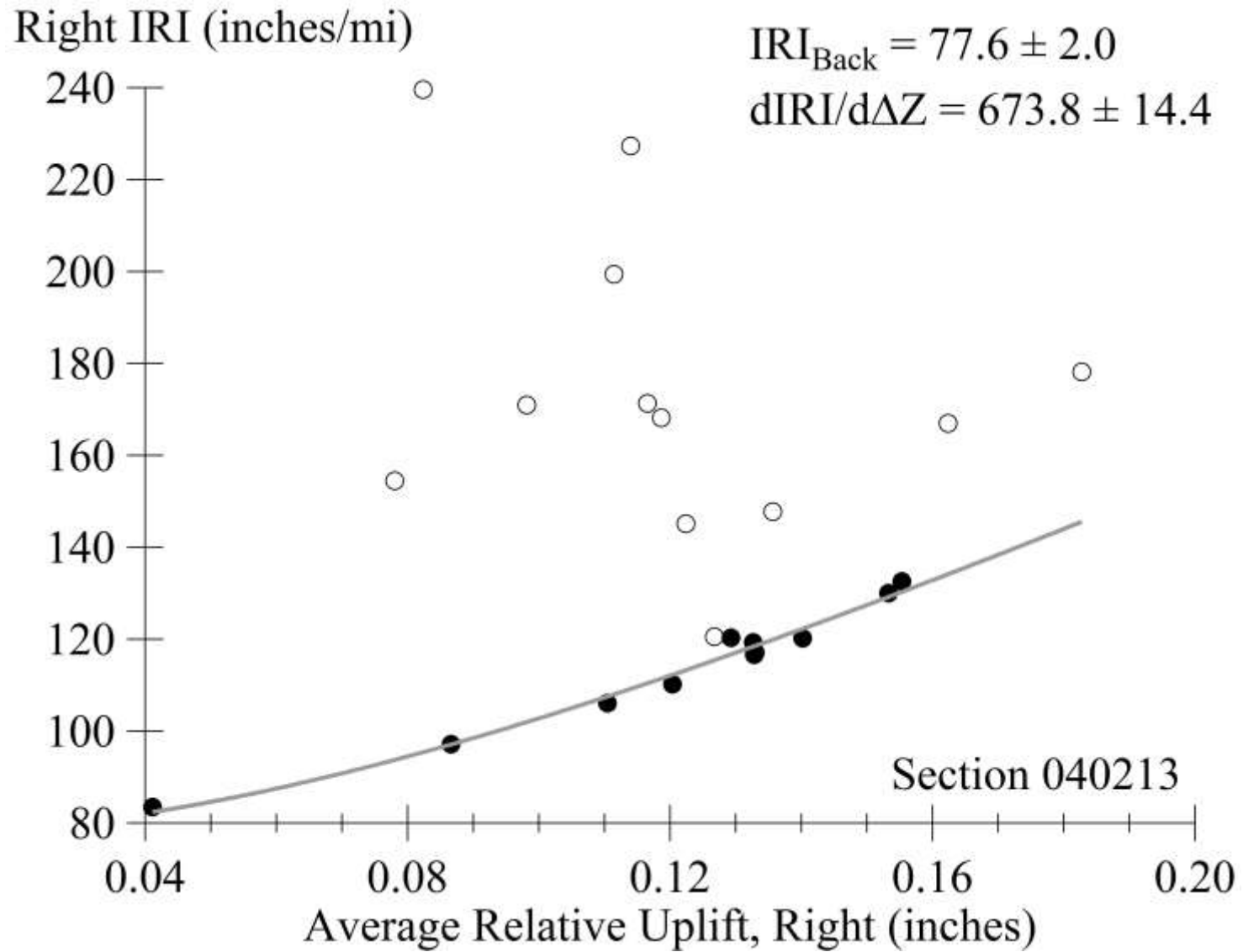
IRI versus Uplift, FHWA Data



IRI versus Uplift, LTPP Data



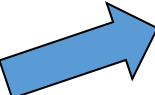
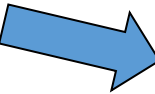
IRI versus Uplift, LTPP Data

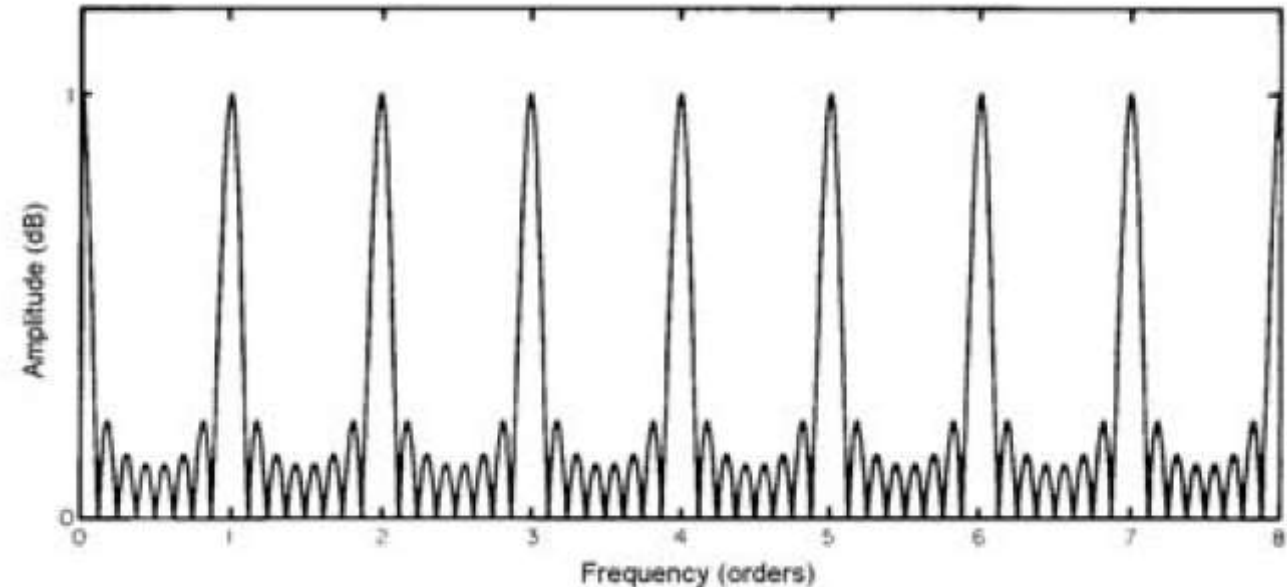
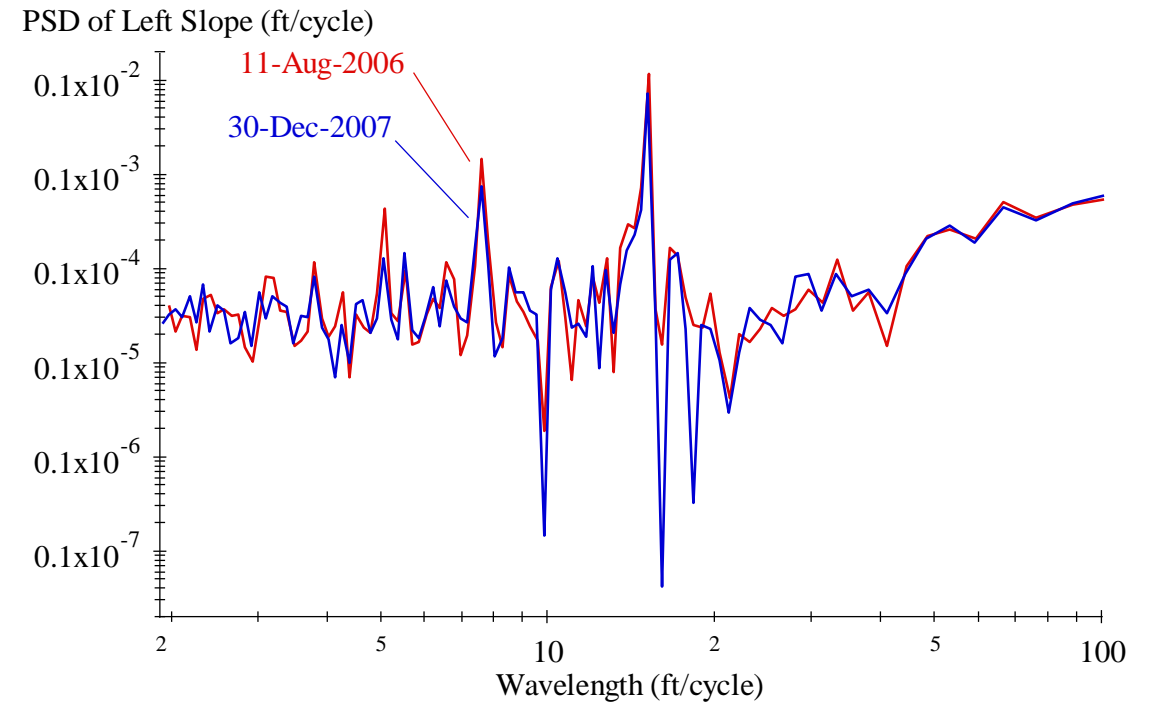


Assessment

- The fitted values relating IRI to uplift were not systematically related to the theory.
- This could be caused by:
 - The structural model.
 - The “sum of squares” model.
 - The low number of slabs per section.
 - Some other thing I haven’t noticed.

Possible Next Steps...

- Notice something new.
- Difference profiles.
- Spectral methods. 
- Specialized filters. 
- “Advanced” methods.



The Report.....
is in the editing phase.

Thank you!!!!